

AN ASYMPTOTICAL METHOD FOR DETERMINING THE COEFFICIENT OF HYDRAULIC RESISTANCE IN GAS-LIFT PROCESS BY THE LINES METHOD*

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Abstract. In the paper the identification problem is considered to determine the coefficient of hydraulic resistance in gas-lift process by the lines method. There exists a small parameter ε in the right side of the partial differential equation of hyperbolic type which is the inverse of the well depth l . Using the lines method the system of partial differential equations of hyperbolic type is reduced to the system of linear ordinary differential equations with respect to the volume of gas, gas liquid mixture (GLM) and their pressure. An asymptotical solution of the given equation is obtained and this solution is calculated at the point $2l$ (debit). On a concrete example is shown that the value of the coefficient of hydraulic resistance obtained by the asymptotical method differs from the real value of the coefficient of hydraulic resistance to the order 10^{-3} .

Keywords: Identification problem, lines method, the coefficient of hydraulic resistance, gas liquid mixture.

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1. Introduction.

The system of partial differential equations of hyperbolic type describing the motions of the gas and gas liquid mixture in the tubes

$z = \frac{x}{|2L|} = \varepsilon x$ is denoted, when a small parameter ε is considered as the inverse of

the well ($\varepsilon = \frac{1}{|2L|}$) depth l ($\varepsilon = \frac{1}{|2L|}$) [1, 7,13,15,21]:

$$\begin{cases} \frac{\partial P}{\partial t} = -\frac{c^2}{F} \frac{\partial Q}{\partial z} \varepsilon, \\ \frac{\partial Q}{\partial t} = -F \frac{\partial P}{\partial z} \varepsilon - 2aQ, \end{cases} \quad (1)$$

where $P = P(x, t)$ – is pressure, $Q(x, t)$ – is volume of gas and GLM, correspondingly, c – is the speed of sound in the gas and GLM, correspondingly;

$2a = \frac{g}{\omega_c} + \frac{\lambda_c \omega_c}{2D}$; g , λ_c – acceleration of gravity and hydraulic resistance in the

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gas and GLM, correspondingly; ω_c - averaged over the cross section of the velocity of the gas and mixture in the annular zone and lift, internal diameters of lift and annular space, which are constant over the axes, F - cross-sectional area of tubing constant on axes. If we denote $l = \frac{1}{2n}$ we obtain from (1) approximately linear model [8, 20] applying the lines method for $n=2$

$$\begin{cases} \dot{P}_1 = -\frac{c_1^2 \varepsilon}{F_1 l} Q_1 + \frac{c_1^2 \varepsilon}{F_1 l} Q_0, \\ \dot{Q}_1 = -\frac{F_1 \varepsilon}{l} P_1 + \frac{F_1 \varepsilon}{l} P_0 - 2a_1 Q_1, \\ \dot{P}_2 = -\frac{c_2^2 \varepsilon}{F_2 l} Q_2 + \frac{c_2^2 \varepsilon}{F_2 l} Q_1 + \frac{c_2^2 \varepsilon}{F_2 l} Q_{pl}, \\ \dot{Q}_2 = -\frac{F_2 \varepsilon}{l} P_2 + \frac{F_2 \varepsilon}{l} P_1 - 2a_2 Q_2 + \frac{F_2 \varepsilon}{l} P_{pl}, \end{cases} \quad (2)$$

where Q_{pl}, P_{pl} are volume flow and pressure of the reservoir at the bottom of the well.

After some transformations the system (2) is reduced to [11, 19]

$$\dot{x} = (A_0(\lambda_c) + A_1 \varepsilon)x + B \varepsilon u + V \varepsilon, \quad (3)$$

with initial condition

$$x_0 = [P_1^0, Q_1^0, P_2^0, Q_2^0]^T,$$

where x_0 is the initial position of the well and

$$A_1 = \begin{bmatrix} 0 & -\frac{c_1^2}{F_1 l} & 0 & 0 \\ -\frac{F_1}{l} & 0 & 0 & 0 \\ 0 & \frac{c_2^2}{F_2 l} & 0 & -\frac{c_2^2}{F_2 l} \\ \frac{F_2}{l} & 0 & -\frac{F_2}{l} & 0 \end{bmatrix}, \quad A_0 = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & -2a_1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -2a_2 \end{bmatrix}, \quad B = \begin{bmatrix} 0 & \frac{c_1^2}{F_1 l} \\ \frac{F_1}{l} & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix},$$

$$V = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & \frac{c_2^2}{F_2 l} \\ \frac{F_2}{l} & 0 \end{bmatrix} \cdot \begin{bmatrix} P_{pl} \\ Q_{pl} \end{bmatrix}, \quad u = \begin{bmatrix} P_0 \\ Q_0 \end{bmatrix}, \quad x = [P_1, Q_1, P_2, Q_2]^T.$$

2. Problem statement. Let's have some statistics that at the given initial volumes of gas \tilde{Q}_0^i the debit \tilde{Q}_2^i is measured at the output, i.e. \tilde{Q}_0^i , and \tilde{Q}_2^i are known ($i = \overline{1, N}$), where N is the number of tests.

It is required to find such values of the coefficient of hydraulic resistance λ_c [3, 4, 12, 18], which system (3) will describe the motion of GLM in the lift, closer to practice (adequate mathematical model). To solve this problem, the objective function based on the lowest square deviation from the real initial data \tilde{Q}_2^i is constructed, i.e. it is required to minimize the functional

$$f(\lambda_c) = \sum_{i=1}^N [\tilde{Q}_2^i - Q_2^i]^2. \tag{4}$$

The analogues problem one can consider for discrete Roesser equation [2].

Thus, the problem of determining the coefficient of hydraulic resistance λ_c can be reduced to finding the gradient of functional (4) [5,6, 9,10, 17].

The general solution of equation (3) can be represented as follows

$$\begin{aligned} x(t) &= e^{(A_0+A_1\varepsilon)t} x_0 + \varepsilon \int_0^t e^{(A_0+A_1\varepsilon)(t-\sigma)} Bud\sigma + \varepsilon \int_0^t e^{(A_0+A_1\varepsilon)(t-\sigma)} Vd\sigma \approx \\ &\approx (E + A_0t + \frac{t^2}{2} A_0^2)x_0 + \varepsilon((A_1t + \frac{t^2}{2} A_0A_1 + \frac{t^2}{2} A_1A_0)x_0 + \\ &+ (Et + \frac{t^2}{2} A_0 + \frac{t^3}{6} A_0^2)(Bu + V)) = x_1 + \varepsilon x_2, \end{aligned} \tag{5}$$

where

$$x_1 = (E + A_0t + \frac{t^2}{2} A_0^2)x_0,$$

$$x_2 = (A_1t + \frac{t^2}{2} A_0A_1 + \frac{t^2}{2} A_1A_0)x_0 + (Et + \frac{t^2}{2} A_0 + \frac{t^3}{6} A_0^2)(Bu + V).$$

After the following transformation

$$A_0 = A_2 + \lambda_c A_3,$$

where

$$A_2 = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & -2a_1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \frac{g}{\omega_c} \end{bmatrix}, \quad A_3 = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -\frac{\omega_c}{2D} \end{bmatrix},$$

the solution (5) is represented as follows

$$x(t) = (E + (A_2 + \lambda_c A_3)t + \frac{t^2}{2}(A_2 + \lambda_c A_3)^2)x_0' + \varepsilon((A_1 t + \frac{t^2}{2}(A_2 + \lambda_c A_3)A_1 + \frac{t^2}{2}A_1(A_2 + \lambda_c A_3))x_0' + (Et + \frac{t^2}{2}(A_2 + \lambda_c A_3) + \frac{t^3}{6}(A_2 + \lambda_c A_3)^2)(Bu + V)). \quad (6)$$

From (6) Q_2 has the form

$$Q_2 = J \cdot x(t), \quad (7)$$

where $J = [0, 0, 0, 1]$, E - is the identity matrix of the corresponding dimension.

Then, substituting (6) and (7) in (4) we have

$$f(\lambda_c) = \sum_{i=1}^N (\tilde{Q}_2^i - Q_2^i)^2 = \sum_{i=1}^N (\tilde{Q}_2^i - Jx(T))^2 = \sum_{i=1}^N (\tilde{Q}_2^i - Jx_1 - \varepsilon Jx_2)^2. \quad (8)$$

$f(\lambda_c)$ from (8) takes the following form throwing the members in which the degree of ε is greater than 1

$$f(\lambda_c) = \sum_{i=1}^N (\tilde{Q}_2^i - Jx_1)^2 - 2\varepsilon \sum_{i=1}^N (\tilde{Q}_2^i - Jx_1)Jx_2 = f_1(\lambda_c) + \varepsilon f_2(\lambda_c) \quad (9)$$

with accuracy $O(\varepsilon^2)$, where

$$\left\{ \begin{aligned} f_1(\lambda_c) &= \sum_{i=1}^N (\tilde{Q}_2^i - Jx_1)^2 = \\ &= \sum_{i=1}^N \left[\tilde{Q}_2^i - J(E + (A_2 + \lambda_c A_3)T + \frac{T^2}{2}(A_2 + \lambda_c A_3)^2)x_0' \right]^2, \\ f_2(\lambda_c) &= -2 \sum_{i=1}^N (\tilde{Q}_2^i - Jx_1)Jx_2 = \\ &= -2 \sum_{i=1}^N \left(\tilde{Q}_2^i - J(E - (A_2 + \lambda_c A_3)T + \frac{T^2}{2}(A_2 + \lambda_c A_3)^2)x_0' \right) J \times \\ &\times \left((A_1 T + \frac{T^2}{2}(A_2 + \lambda_c A_3)A_1 + \frac{T^2}{2}A_1(A_2 + \lambda_c A_3))x_0' + (TE + \frac{T^2}{2}(A_2 + \lambda_c A_3) + \right. \\ &\left. + \frac{T^3}{6}(A_2 + \lambda_c A_3)^2)(Bu + V) \right). \end{aligned} \right. \quad (10)$$

To solve the initial optimization problem we find the gradient of the functional $f(\lambda_c)$ as

$$\frac{\partial f}{\partial \lambda_c} = \left(\frac{\partial f_1}{\partial \lambda_c} + \frac{\partial f_2}{\partial \lambda_c} \varepsilon \right) \cdot \delta \lambda$$

and consider the equation

$$\frac{\partial f(\lambda_c)}{\partial \lambda_c} = 0, \tag{11}$$

for satisfying the last equation we have the following relations

$$\frac{\partial f_1(\lambda_c)}{\partial \lambda_c} = 0, \quad \frac{\partial f_2(\lambda_c)}{\partial \lambda_c} = 0. \tag{12}$$

The relation (9) allows one to solve the system of algebraic equations (12) analytically, if λ_c sought in the form [14, 16]

$$\lambda_c = \lambda_0 + \varepsilon \lambda_1 + \dots,$$

i.e. calculating the equation $\frac{\partial f_1(\lambda_c)}{\partial \lambda_c} = 0$ we have

$$\begin{aligned} \frac{\partial f_1(\lambda_c)}{\partial \lambda_c} = & -2 \sum_{i=1}^N [\tilde{Q}_2^i - J(E + A_2 T + \lambda_c A_3 T + \frac{T^2}{2} A_2^2 + \frac{T^2}{2} \lambda_c A_2 A_3 + \frac{T^2}{2} \lambda_c A_3 A_2 + \\ & + \frac{T^2}{2} \lambda_c^2 A_3^2) x_0^i] J(A_3 T - T^2 A_2 A_3 - T^2 \lambda_c A_3^2) x_0^i = 0. \end{aligned} \tag{13}$$

After some transformations in the equation (13) we obtain the following relation for λ_0

$$\begin{aligned} & \lambda_0^3 \sum_{i=1}^N J \frac{T^2}{2} A_3^2 J' x_0^i T^2 A_3^2 x_0^i + \lambda_0^2 - \left(\sum_{i=1}^N J(A_3 T + \frac{T^2}{2} A_2 A_3 + \frac{T^2}{2} A_3 A_2) J' x_0^i T^2 A_3^2 x_0^i - \right. \\ & \left. - J \frac{T^2}{2} A_3^2 J' x_0^i (A_3 T - T^2 A_2 A_3) x_0^i \right) + \lambda_0 \left(\sum_{i=1}^N J(E + A_2 T + \frac{T^2}{2} A_2^2) J' x_0^i T^2 A_3^2 x_0^i - \right. \\ & \left. - J(A_3 T + \frac{T^2}{2} A_2 A_3 + \frac{T^2}{2} A_3 A_2) J' x_0^i (A_3 T - T^2 A_2 A_3) x_0^i - \tilde{Q}_2^i J T^2 A_3^2 x_0^i \right) + \\ & \left. + \left(\sum_{i=1}^N \tilde{Q}_2^i J(A_3 T - T^2 A_2 A_3) x_0^i - J(E + A_2 T + \frac{T^2}{2} A_2^2) J' x_0^i (A_3 T - T^2 A_2 A_3) x_0^i \right) = 0. \end{aligned} \tag{14}$$

Let's calculate $\frac{\partial f_2(\lambda_c)}{\partial \lambda_c} = 0$

$$\begin{aligned} \frac{\partial f_2(\lambda_c)}{\partial \lambda_c} = & -2 \sum_{i=1}^N \left((JA_3 T - JT^2(A_2 + \lambda_c A_3)A_3) x_0^i \right) J \left((A_1 T + \frac{T^2}{2} (A_2 + \lambda_c A_3) A_1 + \right. \\ & \left. + \frac{T^2}{2} A_1 (A_2 + \lambda_c A_3)) x_0^i + (TE + \frac{T^2}{2} (A_2 + \lambda_c A_3) + \frac{T^3}{6} (A_2 + \lambda_c A_3)^2) (Bu + V) \right) - \\ & - 2 \sum_{i=1}^N \left(\tilde{Q}_2^i - J(E - (A_2 + \lambda_c A_3)T + \frac{T^2}{2} (A_2 + \lambda_c A_3)^2) x_0^i \right) J \times \end{aligned}$$

$$\times \left(\left(\frac{T^2}{2} A_3 A_1 + \frac{T^2}{2} A_1 A_3 \right) x_0^i + \left(\frac{T^2}{2} A_3 + \frac{T^3}{3} (A_2 + \lambda_c A_3) A_3 \right) (Bu + V) \right). \quad (15)$$

From (15) we may define λ_1 as follows

$$\begin{aligned} & - \sum_{i=1}^N \left((JA_3 T - \lambda_0 J T^2 A_2 A_3 - \varepsilon \lambda_1 J T^2 A_3^2) x_0^i \right) J \left((A_1 T + \frac{T^2}{2} A_2 A_1 + \lambda_0 \frac{T^2}{2} A_3 A_1 + \right. \\ & + \varepsilon \lambda_1 \frac{T^2}{2} A_3 A_1 + \frac{T^2}{2} A_1 A_2 + \lambda_0 \frac{T^2}{2} A_1 A_3 + \varepsilon \lambda_1 \frac{T^2}{2} A_3 A_1) x_0^i + (TE + \frac{T^2}{2} A_2 + \lambda_0 \frac{T^2}{2} A_3 + \\ & + \varepsilon \lambda_1 \frac{T^2}{2} A_3 + \frac{T^3}{6} A_2^2 + \lambda_0 \frac{T^3}{6} A_2 A_3 + \varepsilon \lambda_1 \frac{T^3}{6} A_2 A_3 + \lambda_0 \frac{T^3}{6} A_3 A_2 + \varepsilon \lambda_1 \frac{T^3}{6} A_3 A_2 + \\ & + \frac{T^3}{6} \lambda_0^2 A_3^2 + \frac{T^3}{3} \varepsilon \lambda_0 \lambda_1 A_3^2) (Bu + V) - \\ & - \sum_{i=1}^N (\tilde{Q}_2^i - J(E - A_2 T - \lambda_0 A_3 T - \varepsilon \lambda_1 A_3 T + \frac{T^2}{2} \lambda_0 A_2 A_3 + \varepsilon \lambda_1 \frac{T^2}{2} A_2 A_3 + \lambda_0 \frac{T^2}{2} A_3 A_2 + \\ & + \varepsilon \lambda_1 \frac{T^2}{2} A_3 A_2 + \lambda_0^2 \frac{T^2}{2} A_3^2 + \varepsilon \lambda_0 \lambda_1 T^2 A_3^2 + \varepsilon^2 \lambda_1^2 A_3^2) x_0^i) J \left(\left(\frac{T^2}{2} A_3 A_1 + \frac{T^2}{2} A_1 A_3 \right) x_0^i + \right. \\ & \left. + \left(\frac{T^2}{2} A_3 + \frac{T^3}{3} A_2 A_3 + \lambda_0 \frac{T^3}{3} A_3^2 + \varepsilon \lambda_1 \frac{T^3}{3} A_3^2 \right) (Bu + V) \right) = 0. \quad (16) \end{aligned}$$

Thus, we formulate the following algorithm for finding λ_c .

Algorithm.

1. Entering the initial data and parameters from (3);
2. Entering the x_0 , the statistical data \tilde{Q}_0^i and observations \tilde{Q}_2^i from the practice for the same well;
3. Finding $x(t)$ from (6);
4. Forming the functional $f(a_2(\lambda_c))$ from (9), i.e. finding $f_1(\lambda_c)$ and $f_2(\lambda_c)$ from (10)
5. Finding λ_0 and λ_1 from (14), (16) to define the solution of the equation (11)
6. For sufficiently small number ε we check the condition $\left| \frac{\partial f(a_2(\lambda_c))}{\partial a_2(\lambda_c)} \right| < \varepsilon$:
if it is satisfied, the calculations stop, otherwise go to step 2.

Now consider the realization of the proposed algorithm. Let parameters in (5) have the following form

For $0 \leq x < l - 0$:

$$l = 1485m, \quad c_1 = 331m / san, \quad \rho_1 = 0.717kg / m^3, \quad d_1 = \sqrt{114^2 - 73^2} \cdot 10^{-3} m, \quad \lambda_1 = 0.01;$$

for $l + 0 < x \leq 2l$:

$$c_2 = 850m / san, \quad \rho_2 = 700kg / m^3, \quad d_2 = 0.073m, \quad \lambda_2 = 0.23.$$

$$A = \begin{bmatrix} 0 & -12252.2 & 0 & 0 \\ -4.05498 \cdot 10^{-6} & -2.9791131 & 0 & 0 \\ 0 & 1.162454 \cdot 10^5 & 0 & -1.162454 \cdot 10^5 \\ 2.818442 \cdot 10^{-6} & 0 & -2.818442 \cdot 10^{-6} & 1.795454 \cdot 10^2 \end{bmatrix},$$

$$B = \begin{bmatrix} 0 & 1.22522 \cdot 10^4 \\ 4.054981 \cdot 10^{-6} & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}, V = \begin{bmatrix} 0 \\ 0 \\ 1.162454 \cdot 10^7 \\ 2.8184422 \cdot 10^{-4} \end{bmatrix}.$$

After applying of the proposed algorithm we obtain that $\lambda_0 = 0.2373191$, $\lambda_1 = -15.19319$, here $\lambda_c = 0.2373198$ and $\tilde{\lambda}_c = 0.23$ ($\tilde{\lambda}_c$ the hydraulic resistance value from practice), Note that λ_c differs from $\tilde{\lambda}_c$ to the order 10^{-3} , and it shows the efficiency of the proposed algorithm.

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